



<http://elec3004.org>

Digital Filters

ELEC 3004: Digital Linear Systems: Signals & Controls

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Lecture 7

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Schedule

Week	Date	Lecture Title
1	2-Mar	Introduction
	3-Mar	Systems Overview
2	9-Mar	Signals as Vectors & Systems as Maps
	10-Mar	[Signals]
3	16-Mar	Sampling & Data Acquisition & Antialiasing Filters
	17-Mar	[Sampling]
4	23-Mar	System Analysis & Convolution
	24-Mar	[Convolution & FT]
5	30-Mar	Discrete Systems & Z-Transforms
	31-Mar	[Z-Transforms]
6	13-Apr	Frequency Response & Filter Analysis
	14-Apr	[Filters]
7	20-Apr	Digital Filters
	21-Apr	[Digital Filters]
8	27-Apr	Introduction to Digital Control
	28-Apr	[Feedback]
9	4-May	Digital Control Design
	5-May	[Digital Control]
10	11-May	Stability of Digital Systems
	12-May	[Stability]
11	18-May	State-Space
	19-May	Controllability & Observability
12	25-May	PID Control & System Identification
	26-May	Digital Control System Hardware
13	31-May	Applications in Industry & Information Theory & Communications
	2-Jun	Summary and Course Review



ELEC 3004: Systems

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➔ Digital Filters

- Wikipedia Says:

A **digital filter** is a system that performs mathematical operations on a [sampled, discrete-time signal](#) to reduce or enhance certain aspects of that signal.

- Basically we have a transfer function or ... a difference equation

In the Z-domain:

$$H(z) = \frac{B(z)}{A(z)} = \frac{b_0 + b_1 z^{-1} + b_2 z^{-2} + \dots + b_N z^{-N}}{1 + a_1 z^{-1} + a_2 z^{-2} + \dots + a_M z^{-M}}$$

- This is a recursive form with inputs (Numerator) and outputs (Denominator)
➔ “IIR infinite impulse response” behaviour
- If the denominator is made equal to unity (i.e. no feedback)
➔ then this becomes an FIR or finite impulse response filter.



Flashback: LCC Difference Equations

- Start with: $\sum_{k=0}^N a_k \frac{d^k y(t)}{dt^k} = \sum_{k=0}^M b_k \frac{d^k x(t)}{dt^k}$
 - **N**: Highest derivative of the output $y(t)$
 - **M**: Highest derivative of the input $x(t)$
- $\sum_{k=0}^N a_k y[n - k] = \sum_{k=0}^M b_k x[n - k]$
- Solution strategy: Find the particular solution to:
 $\sum_{k=0}^N a_k y[n - k] = 0$
- Leads to a Recursive Equation:
$$y[n - k] = \frac{1}{a_0} \{ \sum_{k=0}^M b_k x[n - k] - \sum_{k=0}^N a_k y[n - k] \}$$

➔ If $N=0$: Non-Recursive Solution:
$$y[n] = \sum_{k=0}^M \left(\frac{b_k}{a_0} \right) x[n - k]$$



Flashback: Two Types of Systems

- Linear shift-invariant:

$$y = \sum_{k=0}^{N-1} u[k] Z^k h$$

Z: Shift operator

$$Z \cdot [u_0, u_1, u_2, u_3, \dots, u_{n-1}]^T = [u_{n-1}, u_0, u_1, u_2, \dots, u_{n-2}]^T$$

- Linear time-invariant system

$$y = \sum_{k=-\infty}^{\infty} u[k] R^k h$$

R: Unit delay operator

$$R \cdot [\dots, u_0, u_1, u_2, u_3, \dots]^T = [\dots, u_{-1}, u_0, u_1, \dots]^T$$



Flashback: Impulse Response of Both Types

$$y[n] = \frac{1}{2}u[n-1] + \frac{1}{2}u[n]$$

$$y[-1] = 0$$

$$y[0] = \frac{1}{2}$$

$$y[1] = \frac{1}{2}$$

$$y[2] = 0$$

\vdots

$$y[n] = \frac{1}{2}y[n-1] + u[n]$$

$$h[-1] = 0$$

$$h[0] = 1$$

$$h[1] = \frac{1}{2}$$

$$h[2] = \frac{1}{4}$$

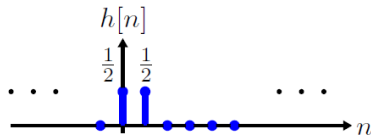
\vdots

$$h[n] = \begin{cases} 0 & n < 0 \\ (\frac{1}{2})^n & n \geq 0 \end{cases}$$



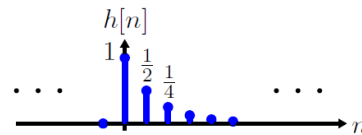
Flashback: Impulse Response of Both Types

$$y[n] = \frac{1}{2}u[n-1] + \frac{1}{2}u[n]$$



“Finite impulse response” (FIR)

$$y[n] = \frac{1}{2}y[n-1] + u[n]$$



“Infinite impulse response” (IIR)



→ Digital Filters Types

FIR

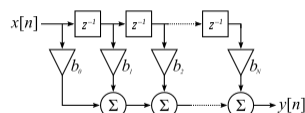
From $H(z)$:

$$\begin{aligned} \rightarrow H(\omega) &= h_0 + h_1 e^{-i\omega} + \dots + h_{n-1} e^{-i(n-1)\omega} \\ &= \sum_{t=0}^{n-1} h_t \cos t\omega - i \sum_{t=0}^{n-1} h_t \sin t\omega \end{aligned}$$

→ Filter becomes a “multiply, accumulate, and delay” system:

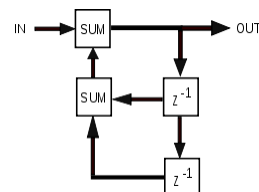
$$y(t) = \sum_{\tau=0}^{n-1} h_{\tau} u(t - \tau)$$

$$y[n] = b_0 x[n] + b_1 x[n-1] + \dots + b_N x[n-N]$$



IIR

- Impulse response function that is non-zero over an infinite length of time.



FIR Properties

- Require no feedback.
 - Are inherently stable.
 - They can easily be designed to be [linear phase](#) by making the coefficient sequence symmetric
 - Flexibility in shaping their magnitude response
 - Very Fast Implementation (based around FFTs)
-
- The main disadvantage of FIR filters is that considerably more computation power in a general purpose processor is required compared to an IIR filter with similar sharpness or [selectivity](#), especially when low frequency (relative to the sample rate) cutoffs are needed.



FIR as a class of LTI Filters

- Transfer function of the filter is

$$H(z) = \frac{Y(z)}{X(z)} = \frac{\sum_{k=0}^M b_k z^{-k}}{1 + \sum_{k=1}^N a_k z^{-k}}$$

- Finite Impulse Response (FIR) Filters: ($N = 0$, no feedback)

→ From $H(z)$:

$$\begin{aligned} H(\omega) &= h_0 + h_1 e^{-i\omega} + \dots + h_{n-1} e^{-i(n-1)\omega} \\ &= \sum_{t=0}^{n-1} h_t \cos t\omega - i \sum_{t=0}^{n-1} h_t \sin t\omega \end{aligned}$$

∴ $H(\omega)$ is periodic and conjugate

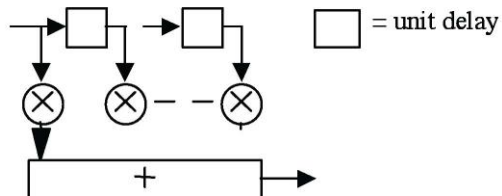
∴ Consider $\omega \in [0, \pi]$



FIR Filters

- Let us consider an FIR filter of length M
- Order $N=M-1$ **(watch out!)**
- Order \rightarrow number of delays

$$y(n) = \sum_{k=0}^{M-1} b_k x(n-k) = \sum_{k=0}^{M-1} h(k) x(n-k)$$



FIR Impulse Response

Obtain the impulse response immediately with $x(n) = \delta(n)$:

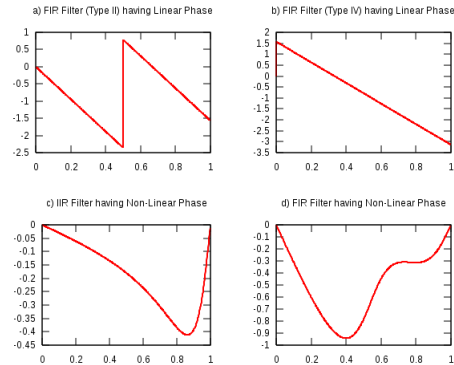
$$h(n) = y(n) = \sum_{k=0}^{M-1} b_k \delta(n-k) = b_n$$

- The impulse response is of finite length M (good!)
- FIR filters have only zeros (no poles) (as they must, $N=0$!!)
 - Hence known also as **all-zero** filters
- FIR filters also known as **feedforward** or **non-recursive**, or **transversal** filters



FIR & Linear Phase

- The [phase response](#) of the filter is a [linear function](#) of [frequency](#)
- Linear phase has constant [group delay](#), all frequency components have equal delay times. \therefore No distortion due to different time delays of different frequencies



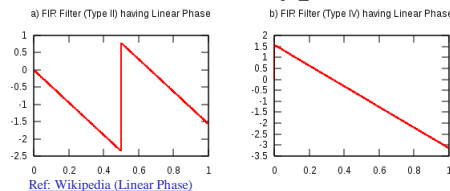
Ref: Wikipedia (Linear Phase)

- FIR Filters with:

$$\sum_{n=-\infty}^{\infty} h[n] \cdot \sin(\omega \cdot (n - \alpha) + \beta) = 0$$



FIR & Linear Phase \rightarrow Four Types



Ref: Wikipedia (Linear Phase)

Impulse response	# coefs	$H(\omega)$	Type
$h(n) = h(M-1-n)$	Odd	$e^{-j\omega(M-1)/2} \left(h\left(\frac{M-1}{2}\right) + 2 \sum_{k=1}^{(M-3)/2} h\left(\frac{M-1}{2} - k\right) \cos(\omega k) \right)$	1
$h(n) = h(M-1-n)$	Even	$e^{-j\omega(M-1)/2} 2 \sum_{k=1}^{(M-2)/2} h\left(\frac{M}{2} - k\right) \cos\left(\omega\left(k - \frac{1}{2}\right)\right)$	2
$h(n) = -h(M-1-n)$	Odd	$e^{-j[\omega(M-1)/2 - \pi/2]} \left(2 \sum_{k=1}^{(M-1)/2} h\left(\frac{M-1}{2} - k\right) \sin(\omega k) \right)$	3
$h(n) = -h(M-1-n)$	Even	$e^{-j[\omega(M-1)/2 - \pi/2]} 2 \sum_{k=1}^{(M-2)/2} h\left(\frac{M}{2} - k\right) \sin\left(\omega\left(k - \frac{1}{2}\right)\right)$	4

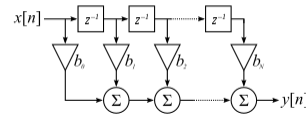
- Type 1: most versatile
- Type 2: frequency response is always 0 at $\omega=\pi$ (not suitable as a high-pass)
- Type 3 and 4: introduce a $\pi/2$ phase shift, 0 at $\omega=0$ (not suitable as a high-pass)



FIR Filter Design

- How to get all these coefficients?

$$H(\omega) = h_0 + h_1 e^{-i\omega} + \dots + h_{n-1} e^{-i(n-1)\omega}$$



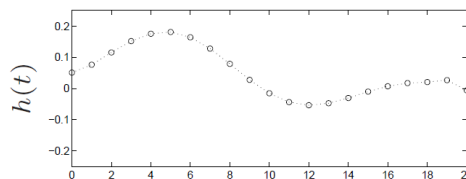
FIR Design Methods:

1. Impulse Response Truncation
 - + Simplest
 - Undesirable frequency domain-characteristics, not very useful
2. Windowing Design Method
 - + Simple
 - Not optimal (not minimum order for a given performance level)
3. Optimal filter design methods
 - + “More optimal”
 - Less simple...

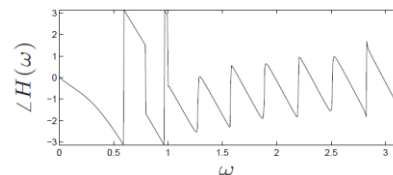
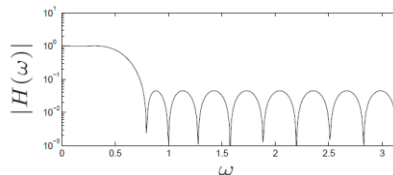
FIR Filter Design & Operation

Ex: Lowpass FIR filter

- Set Impulse response (order $n = 21$)
- “Determine” $h(t)$
 - $h(t)$ is a 20 element vector that we’ll use to as a weighted sum



- FFT (“Magic”) gives $H(\omega)$ Frequency Response & Phase



Why is this “hard”? Looking at the Low-Pass Example

$$H_d(\omega) = \begin{cases} 1 & \text{if } |\omega| \leq \omega_c \\ 0 & \text{if } \omega_c < |\omega| < \pi \end{cases}$$

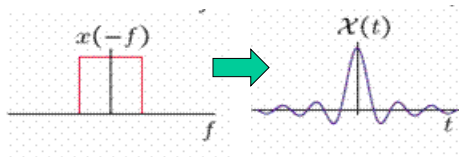
- Why is this hard?
 - Shouldn’t it be “easy” ??
... just hit it with some FFT “magic” and then keep the bands we want and then hit it with some Inverse-FFT “supermagic”???
 - Remember we need a “system” that does this
“rectangle function” in frequency
 - Let’s consider what that means...
 - It basically suggests we need an **Inverse FFT** of a **“rectangle function”**



Flashback: Fourier Series & Rectangular Functions

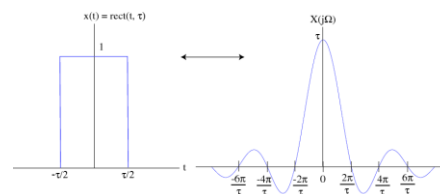
\mathfrak{F} : Fourier Transform

$$\mathfrak{F}^{-1} \left\{ \text{rect} \left(\frac{\omega}{2} \right) \right\} = \frac{\text{sinc}(t)}{\pi}$$



Ref: <http://cnx.org/content/m26719/1.1/>
<http://www.wolframalpha.com/input/?i=-IFFT%28sinc%28%29%29>

$$\mathfrak{F} \{ \text{rect}(t) \} = \text{sinc} \left(\frac{\omega}{2} \right)$$



Ref: <http://cnx.org/content/m32899/1.8/>
<http://www.thefouriertransform.com/pairs/box.php>

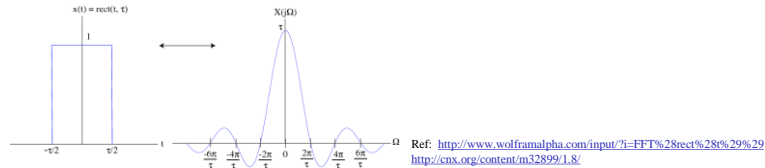
See:

- Table 7.1 (p. 702) Entry 17
& Table 9.1 (p. 852) Entry 7



Flashback: Fourier Series & Rectangular Functions [2]

- The sinc function might look familiar
 - This is the frequency content of a square wave (box)



- This also applies to **signal reconstruction!**
 - **Whittaker–Shannon interpolation formula**
 - This says that the “better way” to go from Discrete to Continuous (i.e. D to A) is not ZOH, but rather via the sinc!

$$x(t) = \sum_{n=-\infty}^{\infty} x[n] \cdot \text{sinc}\left(\frac{t-nT}{T}\right)$$



∴ FIR and Low Pass Filters...

$$\therefore H_d(\omega) = \begin{cases} 1 & \text{if } |\omega| \leq \omega_c \\ 0 & \text{if } \omega_c < |\omega| < \pi \end{cases}$$

Has impulse response:

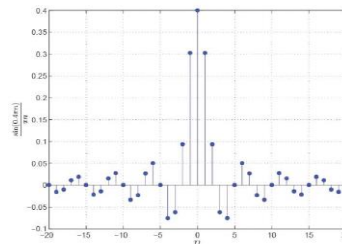
$$h_d(n) = \frac{\omega_c}{\pi} \frac{\sin \omega_c n}{\omega_c n}$$

Thus, to filter an impulse train with an ideal **low-pass filter** use:

$$x(t) = \left(\sum_{n=-\infty}^{\infty} x[n] \cdot \delta(t - nT) \right) * \text{sinc}\left(\frac{t}{T}\right)$$

• **However!!**

a sinc is non-causal and infinite in duration



And, this **cannot** be implemented **in practice** ☹

∴ we need to know all samples of the input, both in the **past** and in the **future**

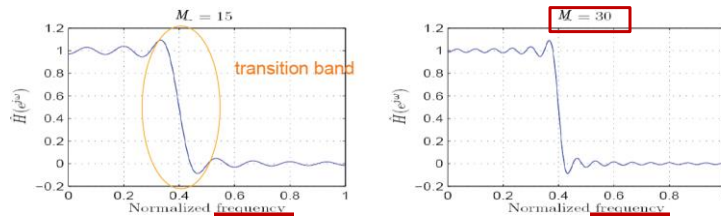


Plan 0: Impulse Response Truncation

Maybe we saw this coming...

∴ Clip off the sinc at some large n

$$\hat{h}(n) = \frac{\sin(n\omega_c)}{\pi n} \text{ for } |n| \leq M \text{ and } 0 \text{ otherwise}$$



- *Ripples* in both passband/stopband and the transition not abrupt (i.e., a *transition band*).
- As $M \rightarrow \infty$, transition band $\rightarrow 0$ (as expected!)



→ FIR Filters: Window Function Design Method

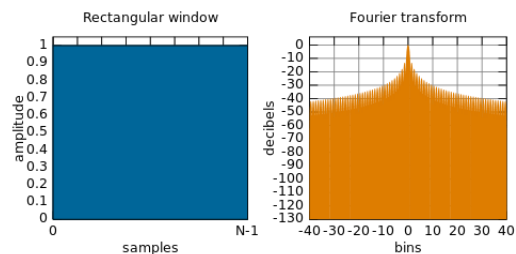
- Windowing: a generalization of the truncation idea
- There many, many “window” functions:
 - Rectangular
 - Triangular
 - Hanning
 - Hamming
 - Blackman
 - Kaiser
 - Lanczos
 - Many More ... (see: http://en.wikipedia.org/wiki/Window_function)



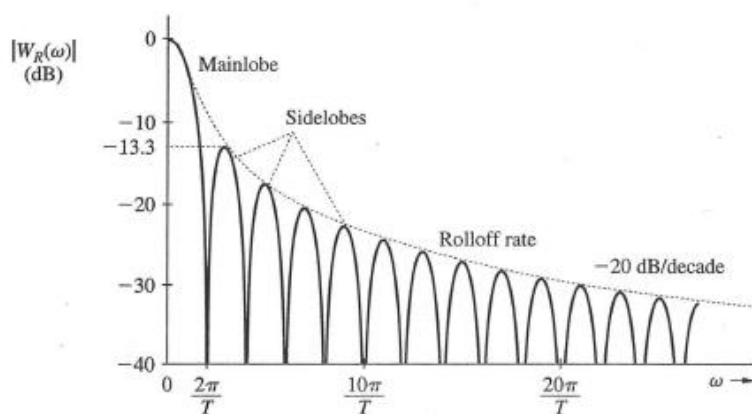
Some Window Functions [1]

1. Rectangular

$$w(n) = 1$$



Windowing and its effects/terminology



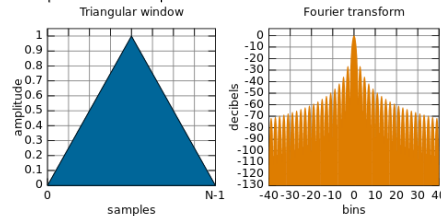
Lathi, Fig. 7.45



Some More Window Functions ...

2. Triangular window

$$w(n) = 1 - \left| \frac{n - \frac{N-1}{2}}{\frac{N-1}{2}} \right|$$



- And Bartlett Windows

- A slightly narrower variant with zero weight at both ends:

$$w(n) = 1 - \left| \frac{n - \frac{N-1}{2}}{\frac{N-1}{2}} \right|$$



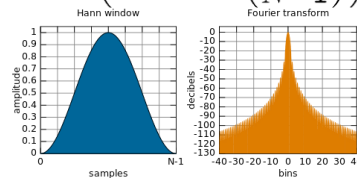
Some More Window Functions...

3. Generalized Hamming Windows

$$w(n) = \alpha - \beta \cos\left(\frac{2\pi n}{N-1}\right)$$

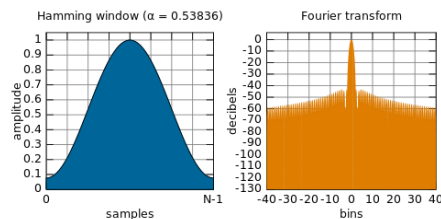
→ Hanning Window

$$\rightarrow w(n) = 0.5 \left(1 - \cos\left(\frac{2\pi n}{N-1}\right) \right)$$



→ Hamming's Window

$$\rightarrow \alpha = 0.54, \beta = 1 - \alpha = 0.46$$

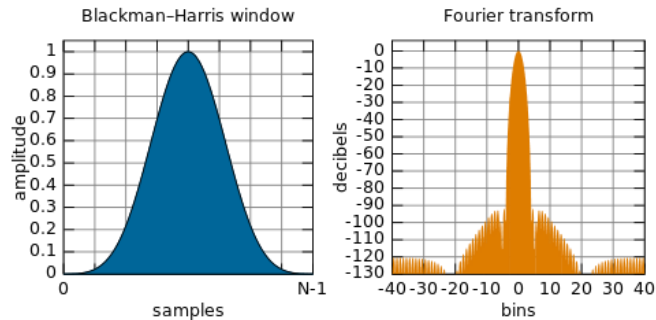


Some More Window Functions...

4. Blackman-Harris Windows

- A generalization of the Hamming family,
- Adds more shifted sinc functions for less side-lobe levels

$$w(n) = a_0 - a_1 \cos\left(\frac{2\pi n}{N-1}\right) + a_2 \cos\left(\frac{4\pi n}{N-1}\right) - a_3 \cos\left(\frac{6\pi n}{N-1}\right)$$



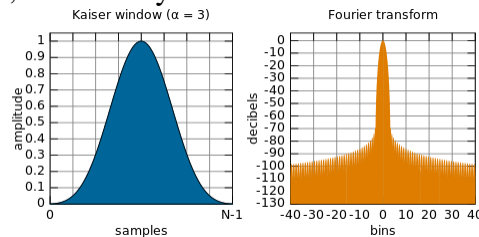
Some More Window Functions...

5. Kaiser window

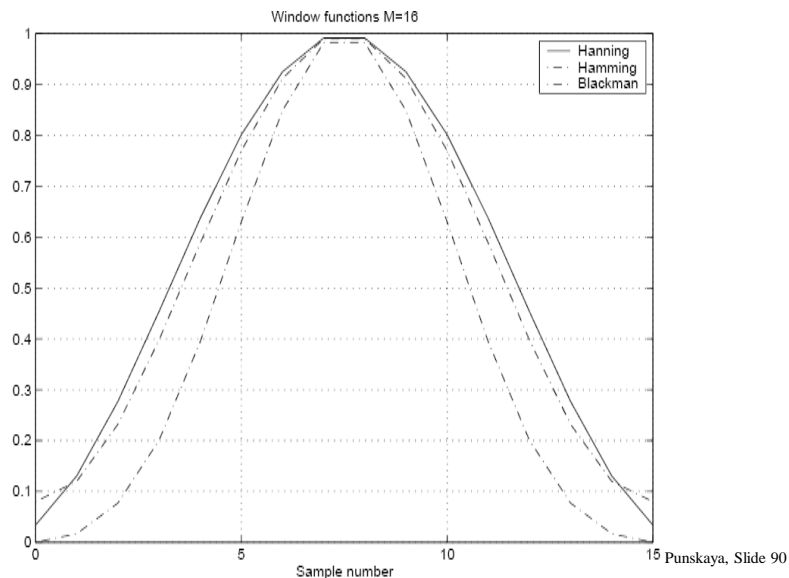
- A DPSS (discrete prolate spheroidal sequence)
- Maximize the energy concentration in the main lobe

$$\rightarrow w(n) = \frac{I_0\left(\pi\alpha\sqrt{1-\left(\frac{2n}{N-1}-1\right)^2}\right)}{I_0(\pi\alpha)}$$

- Where: I_0 is the zero-th order modified Bessel function of the first kind, and usually $\alpha = 3$.

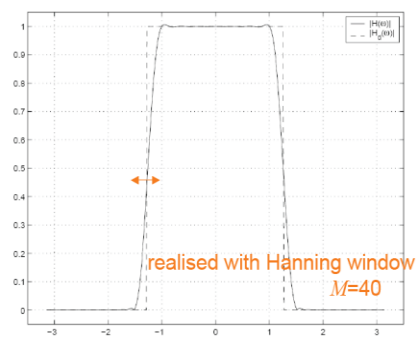
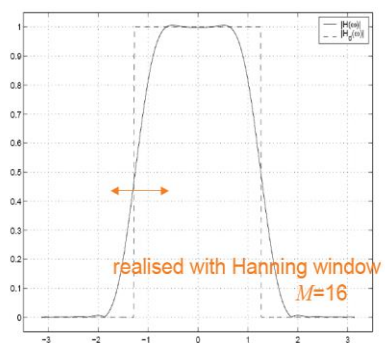


Comparison of Alternative Windows –Time Domain

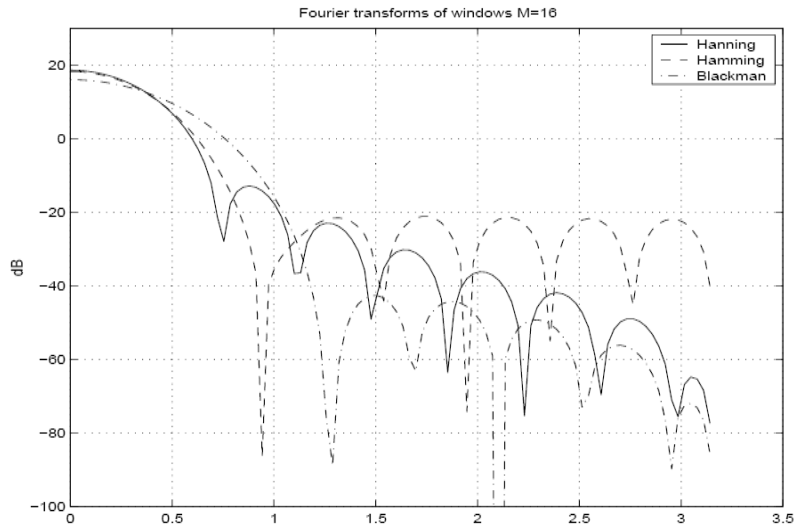


Adding Order

- + Transition and Smoothness
- Increased Size



Comparison of Alternative Windows Frequency Domain



Punskaya, Slide 91



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Summary Characteristics of Common Window Functions

No.	Window $w(t)$	Mainlobe Width	Rolloff Rate (dB/oct)	Peak Sidelobe level (dB)	Peak $20\log_{10}\delta$
1	Rectangular: $\text{rect}\left(\frac{t}{T}\right)$	$\frac{4\pi}{T}$	-6	-13.3	-21dB
2	Bartlett: $\Delta\left(\frac{t}{2T}\right)$	$\frac{8\pi}{T}$	-12	-26.5	
3	Hanning: $0.5 \left[1 + \cos\left(\frac{2\pi t}{T}\right) \right]$	$\frac{8\pi}{T}$	-18	-31.5	-44dB
4	Hamming: $0.54 + 0.46 \cos\left(\frac{2\pi t}{T}\right)$	$\frac{8\pi}{T}$	-6	-42.7	-53dB
5	Blackman: $0.42 + 0.5 \cos\left(\frac{2\pi t}{T}\right) + 0.08 \cos\left(\frac{4\pi t}{T}\right)$	$\frac{12\pi}{T}$	-18	-58.1	-74dB
6	Kaiser: $\frac{I_0\left[\alpha\sqrt{1-4\left(\frac{t}{T}\right)^2}\right]}{I_0(\alpha)}$ $0 \leq \alpha \leq 10$	$\frac{11.2\pi}{T}$	-6	-59.9 ($\alpha = 8.168$)	

Lathi, Table 7.3
Punskaya, Slide 92

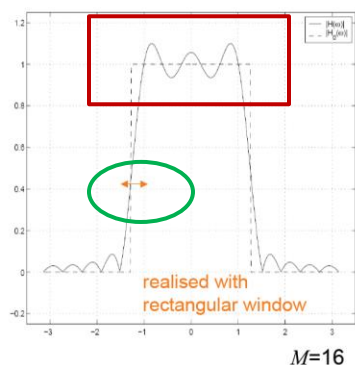


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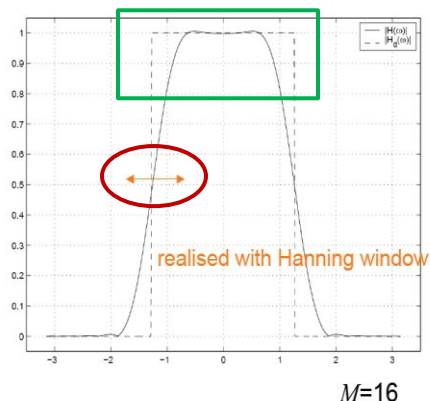
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FIR: Rectangular & Hanning Windows

- Rectangular



- Hanning

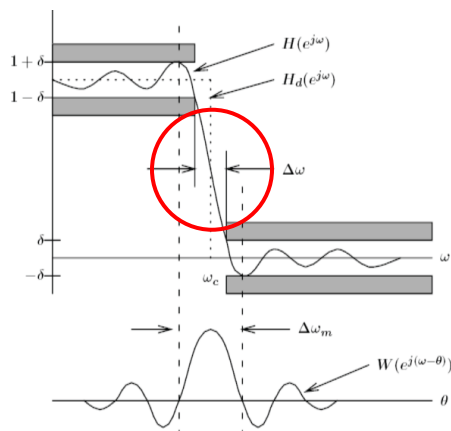


➔ Hanning: Less ripples, but wider transition band

Punskaya, Slide 93



Windowed FIR Property 1: Equal transition bandwidth

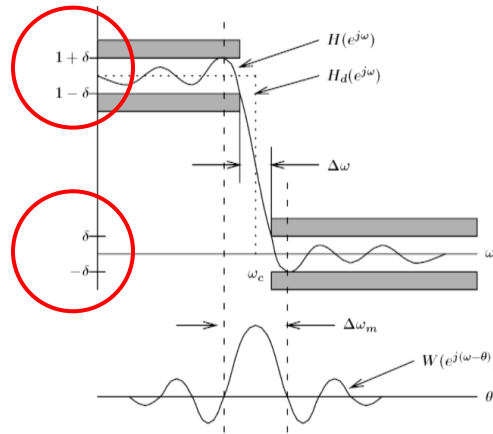


Punskaya, Slide 96

- Equal transition bandwidth on both sides of the ideal cutoff frequency



Windowed FIR Property 2: Peak Errors same in Passband & Stopband

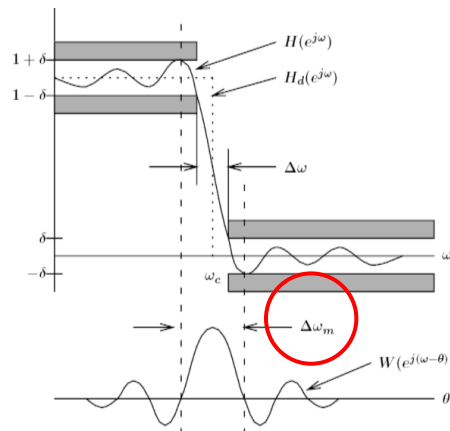


Punskaya, Slide 96

- Peak approximation error in the passband ($1+\delta \rightarrow 1-\delta$) is equal to that in the stopband ($\delta \rightarrow -\delta$)



Windowed FIR Property 3: Mainlobe Width

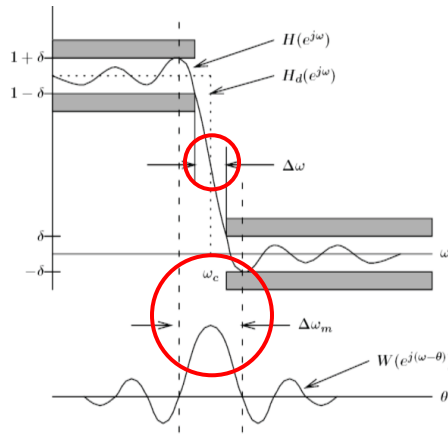


Punskaya, Slide 99

- The distance between approximation error peaks is approximately equal to the width of the mainlobe $\Delta\omega_m$



Windowed FIR Property 4: Mainlobe Width [2]

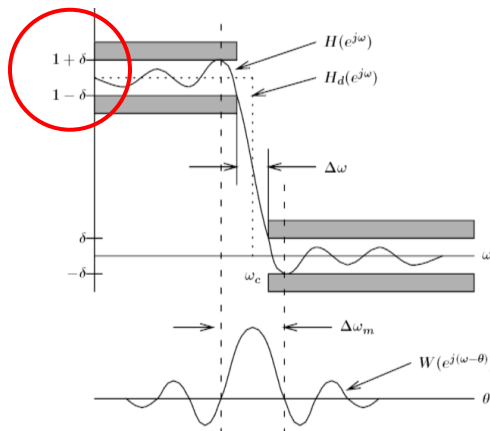


Punskaya, Slide 96

- The width of the mainlobe is wider than the transition bandwidth



Windowed FIR Property 5: Peak $\Delta\delta$ is determined by the window shape



Punskaya, Slide 96

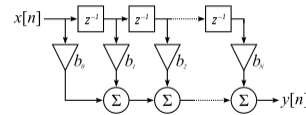
- peak approximation error is determined by the window shape, independent of the filter order



FIR Filter Design

- How to get all these coefficients?

$$H(\omega) = h_0 + h_1 e^{-i\omega} + \dots + h_{n-1} e^{-i(n-1)\omega}$$



FIR Design Methods:

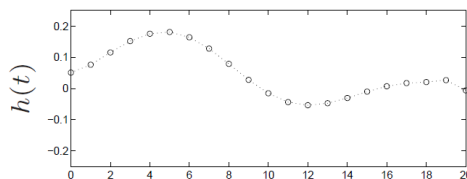
1. Impulse Response Truncation
 - + Simplest
 - Undesirable frequency domain-characteristics, not very useful
2. Windowing Design Method
 - + Simple
 - Not optimal (not minimum order for a given performance level)
3. Optimal filter design methods
 - + “More optimal”
 - Less simple...



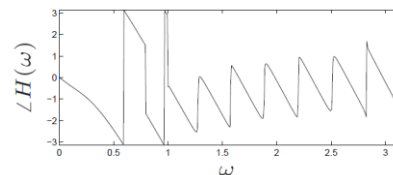
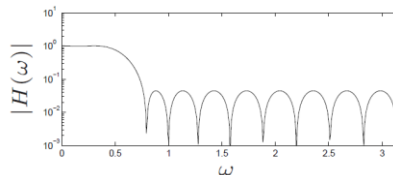
FIR Filter Design & Operation

Ex: Lowpass FIR filter

- Set Impulse response (order $n = 21$)
- “Determine” $h(t)$
 - $h(t)$ is a 20 element vector that we’ll use to as a weighted sum



- FFT (“Magic”) gives $H(\omega)$ Frequency Response & Phase



Why is this “hard”? Looking at the Low-Pass Example

$$H_d(\omega) = \begin{cases} 1 & \text{if } |\omega| \leq \omega_c \\ 0 & \text{if } \omega_c < |\omega| < \pi \end{cases}$$

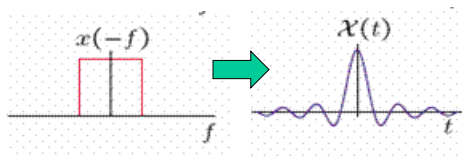
- Why is this hard?
 - Shouldn't it be “easy” ??
... just hit it with some FFT “magic” and then keep the bands we want and then hit it with some Inverse-FFT “supermagic”???
 - Remember we need a “system” that does this
“rectangle function” in frequency
 - Let's consider what that means...
 - It basically suggests we need an **Inverse FFT** of a **“rectangle function”**



Flashback: Fourier Series & Rectangular Functions

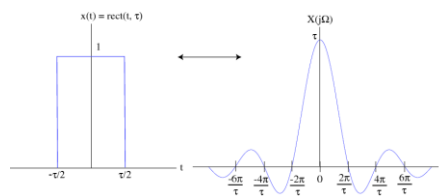
\mathfrak{F} : Fourier Transform

$$\mathfrak{F}^{-1} \left\{ \text{rect} \left(\frac{\omega}{2} \right) \right\} = \frac{\text{sinc}(t)}{\pi}$$



Ref: <http://cnx.org/content/m26719/1.1/>
<http://www.wolframalpha.com/input/?i=IFFT%28sinc%28%29%29>

$$\mathfrak{F} \{ \text{rect}(t) \} = \text{sinc} \left(\frac{\omega}{2} \right)$$



Ref: <http://cnx.org/content/m32899/1.8/>
<http://www.thefouriertransform.com/pairs/box.php>

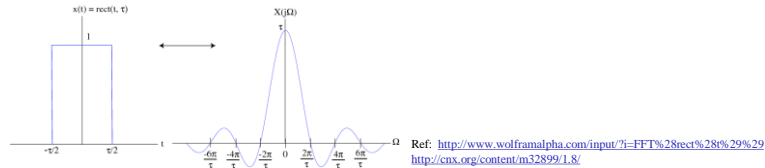
See:

- Table 7.1 (p. 702) Entry 17
& Table 9.1 (p. 852) Entry 7



Flashback: Fourier Series & Rectangular Functions [2]

- The sinc function might look familiar
 - This is the frequency content of a square wave (box)



- This also applies to **signal reconstruction!**
 - **Whittaker–Shannon interpolation formula**
 - This says that the “better way” to go from Discrete to Continuous (i.e. D to A) is not ZOH, but rather via the sinc!

$$x(t) = \sum_{n=-\infty}^{\infty} x[n] \cdot \text{sinc}\left(\frac{t-nT}{T}\right)$$



∴ FIR and Low Pass Filters...

$$\therefore H_d(\omega) = \begin{cases} 1 & \text{if } |\omega| \leq \omega_c \\ 0 & \text{if } \omega_c < |\omega| < \pi \end{cases}$$

Has impulse response:

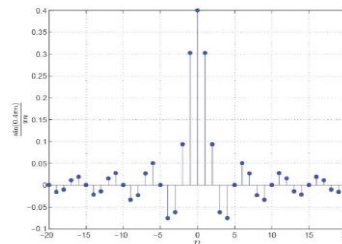
$$h_d(n) = \frac{\omega_c}{\pi} \frac{\sin \omega_c n}{\omega_c n}$$

Thus, to filter an impulse train with an ideal **low-pass filter** use:

$$x(t) = \left(\sum_{n=-\infty}^{\infty} x[n] \cdot \delta(t - nT) \right) * \text{sinc}\left(\frac{t}{T}\right)$$

• **However!!**

a sinc is non-causal and infinite in duration



And, this **cannot** be implemented **in practice** ☹

∴ we need to know all samples of the input, both in the **past** and in the **future**

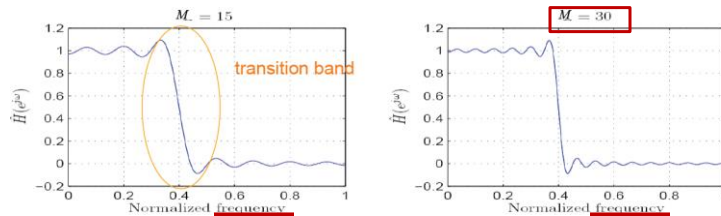


Plan 0: Impulse Response Truncation

Maybe we saw this coming...

∴ Clip off the sinc at some large n

$$\hat{h}(n) = \frac{\sin(n\omega_c)}{\pi n} \text{ for } |n| \leq M \text{ and } 0 \text{ otherwise}$$



- *Ripples* in both passband/stopband and the transition not abrupt (i.e., a *transition band*).
- As $M \rightarrow \infty$, transition band $\rightarrow 0$ (as expected!)



→ FIR Filters: Window Function Design Method

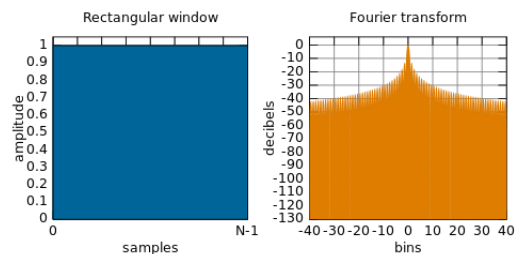
- Windowing: a generalization of the truncation idea
- There many, many “window” functions:
 - Rectangular
 - Triangular
 - Hanning
 - Hamming
 - Blackman
 - Kaiser
 - Lanczos
 - Many More ... (see: http://en.wikipedia.org/wiki/Window_function)



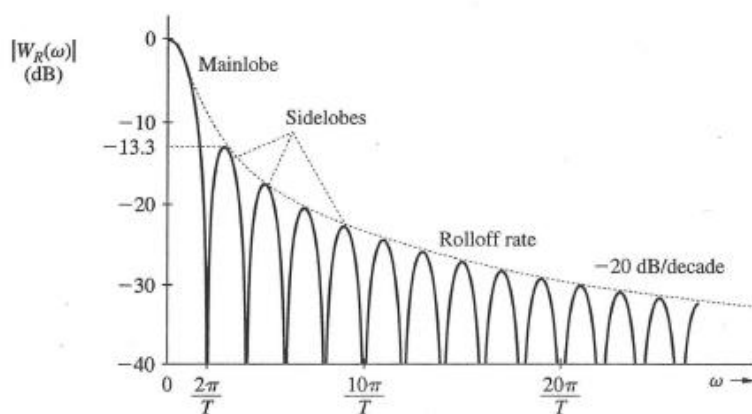
Some Window Functions [1]

1. Rectangular

$$w(n) = 1$$



Windowing and its effects/terminology



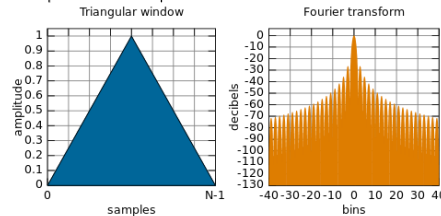
Lathi, Fig. 7.45



Some More Window Functions ...

2. Triangular window

$$w(n) = 1 - \left| \frac{n - \frac{N-1}{2}}{\frac{N-1}{2}} \right|$$



- And Bartlett Windows

- A slightly narrower variant with zero weight at both ends:

$$w(n) = 1 - \left| \frac{n - \frac{N-1}{2}}{\frac{N-1}{2}} \right|$$



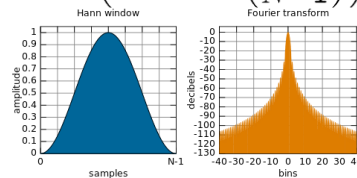
Some More Window Functions...

3. Generalized Hamming Windows

$$w(n) = \alpha - \beta \cos\left(\frac{2\pi n}{N-1}\right)$$

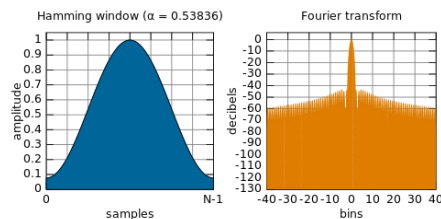
→ Hanning Window

$$\rightarrow w(n) = 0.5 \left(1 - \cos\left(\frac{2\pi n}{N-1}\right) \right)$$



→ Hamming's Window

$$\rightarrow \alpha = 0.54, \beta = 1 - \alpha = 0.46$$

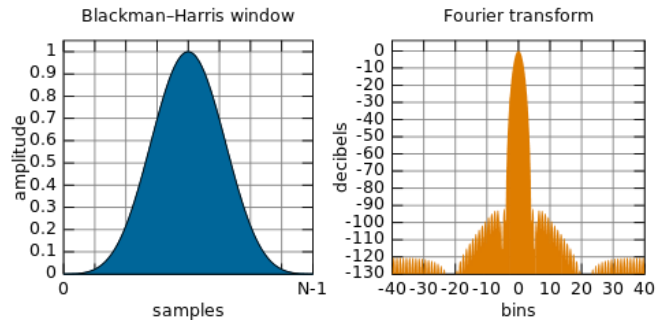


Some More Window Functions...

4. Blackman-Harris Windows

- A generalization of the Hamming family,
- Adds more shifted sinc functions for less side-lobe levels

$$w(n) = a_0 - a_1 \cos\left(\frac{2\pi n}{N-1}\right) + a_2 \cos\left(\frac{4\pi n}{N-1}\right) - a_3 \cos\left(\frac{6\pi n}{N-1}\right)$$



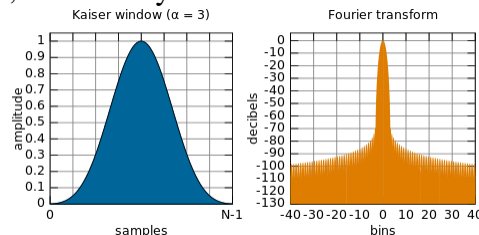
Some More Window Functions...

5. Kaiser window

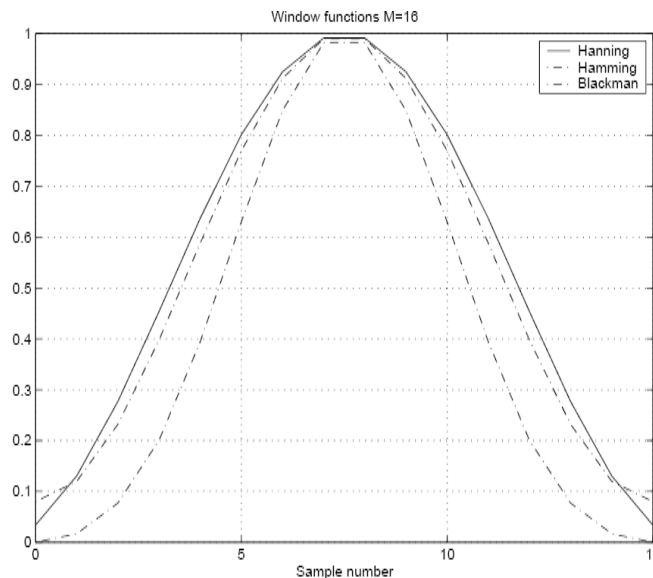
- A DPSS (discrete prolate spheroidal sequence)
- Maximize the energy concentration in the main lobe

$$\rightarrow w(n) = \frac{I_0\left(\pi\alpha\sqrt{1-\left(\frac{2n}{N-1}-1\right)^2}\right)}{I_0(\pi\alpha)}$$

- Where: I_0 is the zero-th order modified Bessel function of the first kind, and usually $\alpha = 3$.



Comparison of Alternative Windows –Time Domain



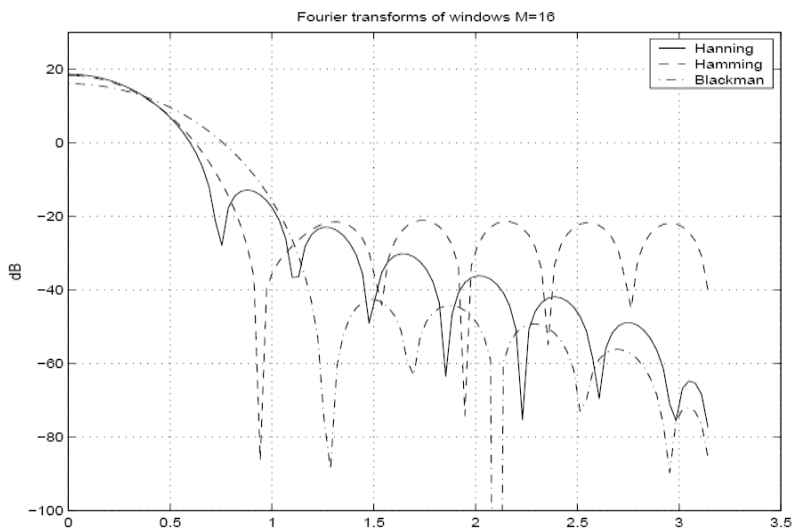
Punskaya, Slide 90



ELEC 3004: Systems

20 April 2015 - 53

Comparison of Alternative Windows Frequency Domain



Punskaya, Slide 91



ELEC 3004: Systems

20 April 2015 - 54

Summary Characteristics of Common Window Functions

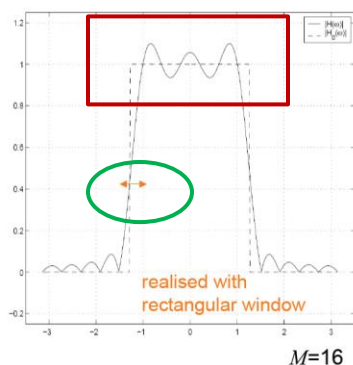
No.	Window $w(t)$	Mainlobe Width	Rolloff Rate (dB/oct)	Peak Sidelobe level (dB)	Peak $20\log_{10}\delta$
1	Rectangular: $\text{rect}\left(\frac{t}{T}\right)$	$\frac{4\pi}{T}$	-6	-13.3	-21dB
2	Bartlett: $\Delta\left(\frac{t}{2T}\right)$	$\frac{8\pi}{T}$	-12	-26.5	
3	Hanning: $0.5 \left[1 + \cos\left(\frac{2\pi t}{T}\right) \right]$	$\frac{8\pi}{T}$	-18	-31.5	-44dB
4	Hamming: $0.54 + 0.46 \cos\left(\frac{2\pi t}{T}\right)$	$\frac{8\pi}{T}$	-6	-42.7	-53dB
5	Blackman: $0.42 + 0.5 \cos\left(\frac{2\pi t}{T}\right) + 0.08 \cos\left(\frac{4\pi t}{T}\right)$	$\frac{12\pi}{T}$	-18	-58.1	-74dB
6	Kaiser: $\frac{I_0\left[\alpha\sqrt{1-4\left(\frac{t}{T}\right)^2}\right]}{I_0(\alpha)}$ $0 \leq \alpha \leq 10$	$\frac{11.2\pi}{T}$	-6	-59.9 ($\alpha = 8.168$)	

Lathi, Table 7.3
Punskeya, Slide 92

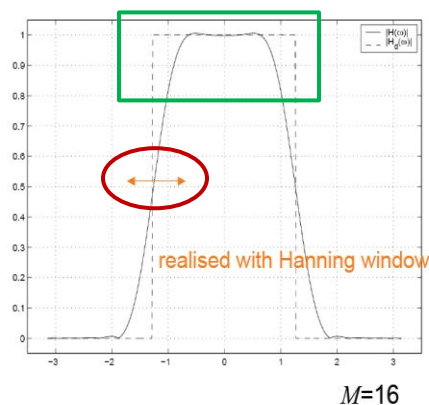


FIR: Rectangular & Hanning Windows

- Rectangular



- Hanning



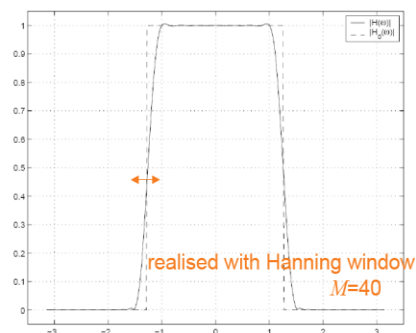
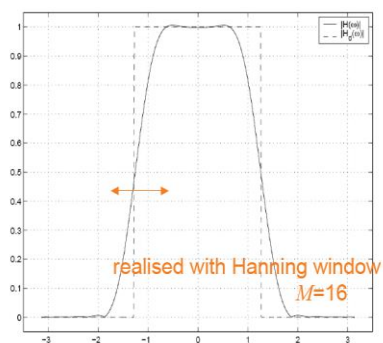
➔ Hanning: Less ripples, but wider transition band

Punskeya, Slide 93



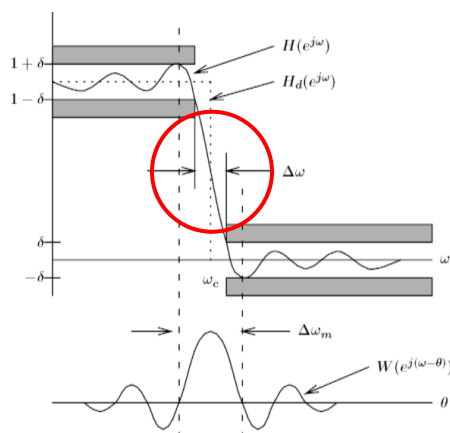
Adding Order

- + Transition and Smoothness
- Increased Size



Punskeya, Slide 94

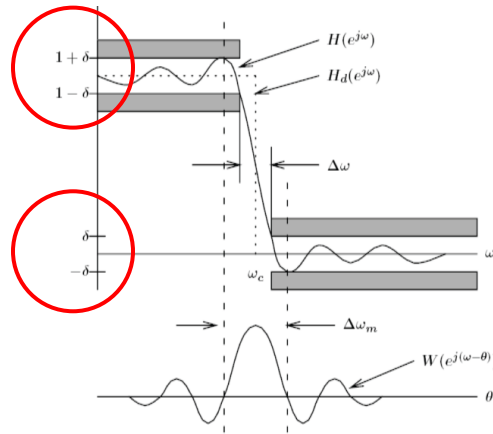
Windowed FIR Property 1: Equal transition bandwidth



Punskeya, Slide 96

- Equal transition bandwidth on both sides of the ideal cutoff frequency

Windowed FIR Property 2: Peak Errors same in Passband & Stopband

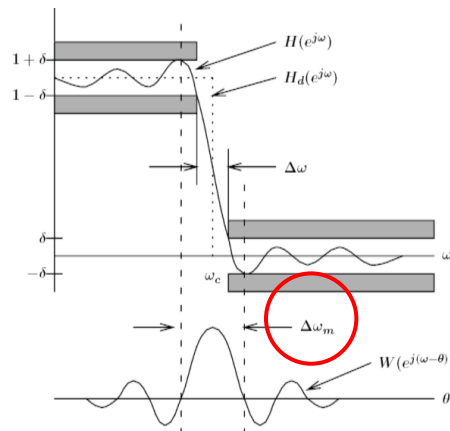


Punskeya, Slide 96

- Peak approximation error in the passband ($1+\delta \rightarrow 1-\delta$) is equal to that in the stopband ($\delta \rightarrow -\delta$)



Windowed FIR Property 3: Mainlobe Width

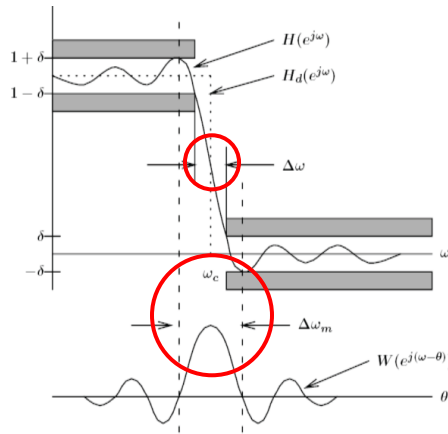


Punskeya, Slide 99

- The distance between approximation error peaks is approximately equal to the width of the mainlobe $\Delta\omega_m$



Windowed FIR Property 4: Mainlobe Width [2]

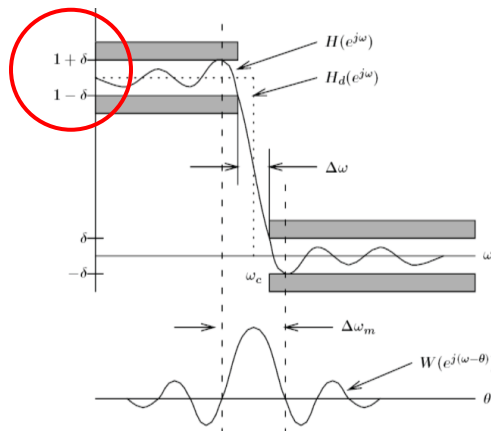


Punskaya, Slide 96

- The width of the mainlobe is wider than the transition bandwidth



Windowed FIR Property 5: Peak $\Delta\delta$ is determined by the window shape

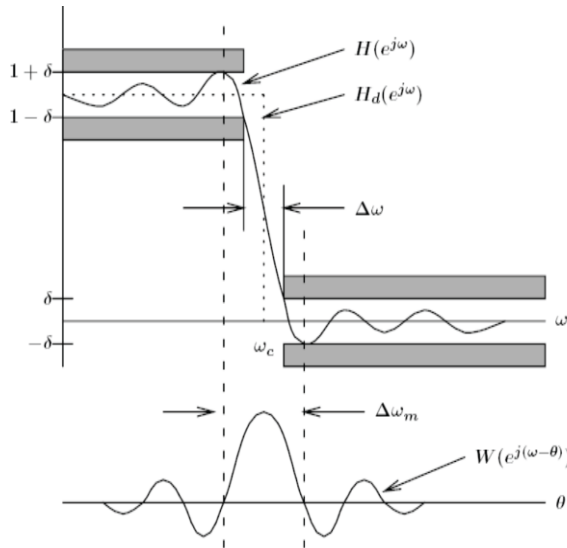


Punskaya, Slide 96

- peak approximation error is determined by the window shape, independent of the filter order



Window Design Method Design Terminology



Where:

- ω_c : cutoff frequency
- δ : maximum passband ripple
- $\Delta\omega$: transition bandwidth
- $\Delta\omega_m$: width of the window mainlobe

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Passband / stopband ripples

ω_s and ω_p : Corner Frequencies

Passband / stopband ripples are often expressed in dB:

- passband ripple = $20 \log_{10} (1 + \delta_p)$ dB
- peak-to-peak passband ripple $\cong 20 \log_{10} (1 + 2\delta_p)$ dB
- minimum stopband attenuation = $-20 \log_{10} (\delta_s)$ dB



Passband / stopband ripples

ω_s and ω_p : Corner Frequencies

Passband / stopband ripples are often expressed in dB:

- passband ripple = ~~$20 \log_{10} (1 + \delta_p)$ dB~~ = $20 \log_{10} (\delta_p)$ dB
- peak-to-peak passband ripple \cong ~~$20 \log_{10} (1 + 2\delta_p)$ dB~~
 $\cong 20 \log_{10} (2\delta_p)$ dB
- minimum stopband attenuation = ~~$20 \log_{10} (\delta_s)$ dB~~
 $= 20 \log_{10} (\delta_s)$ dB



Summary of Design Procedure

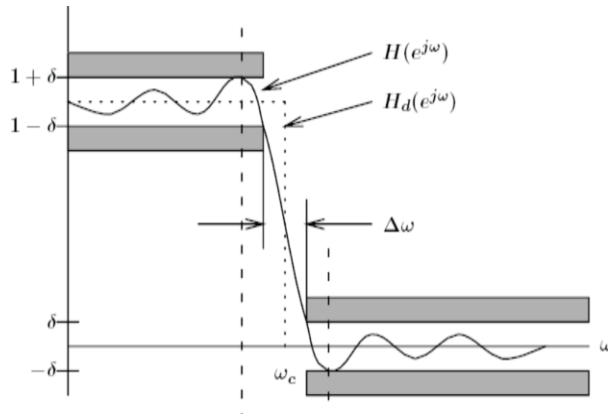
1. Select a suitable window function
2. Specify an ideal response $H_d(\omega)$
3. Compute the coefficients of the ideal filter $h_d(n)$
4. Multiply the ideal coefficients by the window function to give the filter coefficients
5. Evaluate the frequency response of the resulting filter and iterate if necessary (e.g. by increasing M if the specified constraints have not been satisfied).



Windowed Filter Design Example

- Design a type I low-pass filter with:

- $\omega_p = 0.2\pi$
- $\omega_s = 0.3\pi$
- $\delta = 0.01$



Windowed Filter Design Example: Step 1: Select a suitable Window Function

No.	Window $w(t)$	Mainlobe Width	Rolloff Rate (dB/oct)	Peak Sidelobe level (dB)	Peak $20\log_{10}\delta$
1	Rectangular: $\text{rect}\left(\frac{t}{T}\right)$	$\frac{4\pi}{T}$	-6	-13.3	-21dB
2	Bartlett: $\Delta\left(\frac{t}{2T}\right)$	$\frac{8\pi}{T}$	-12	-26.5	
3	Hanning: $0.5\left[1 + \cos\left(\frac{2\pi t}{T}\right)\right]$	$\frac{8\pi}{T}$	-18	-31.5	-44dB
4	Hamming: $0.54 + 0.46\cos\left(\frac{2\pi t}{T}\right)$	$\frac{8\pi}{T}$	-6	-42.7	-53dB
5	Blackman: $0.42 + 0.5\cos\left(\frac{2\pi t}{T}\right) + 0.08\cos\left(\frac{4\pi t}{T}\right)$	$\frac{12\pi}{T}$	-18	-58.1	-74dB
6	Kaiser: $\frac{I_0\left[\alpha\sqrt{1 - 4\left(\frac{t}{T}\right)^2}\right]}{I_0(\alpha)}$ $0 \leq \alpha \leq 10$	$\frac{11.2\pi}{T}$	-6	-59.9 ($\alpha = 8.168$)	

- LP with: $\omega_p = 0.2\pi$, $\omega_s = 0.3\pi$, $\delta = 0.01$

- $\delta = 0.01$: The required peak error spec:
– $20\log_{10}(\delta) = -40$ dB

} Hanning Window

- Main-lobe width:

$$\omega_s - \omega_p = 0.3\pi - 0.2\pi = 0.1\pi \rightarrow 0.1\pi = 8\pi / M$$

\rightarrow Filter length $M \geq 80$ & Filter order $N \geq 79$

- BUT, Type-I filters have even order so **$N = 80$**



Windowed Filter Design Example: Step 2: Specify the Ideal Response

- From Property 1 (Midpoint rule)

→ $\omega_c = (\omega_s + \omega_p)/2 = (0.2\pi + 0.3\pi)/2 = 0.25\pi$

∴ An ideal response will be:

$$H_d(\omega) = \begin{cases} 1 & \text{if } |\omega| \leq 0.25\pi \\ 0 & \text{if } 0.25\pi < |\omega| < \pi \end{cases}$$



Windowed Filter Design Example: Step 3: Compute the coefficients of the ideal filter

- The ideal filter coefficients h_d are given by the Inverse **Discrete time** Fourier transform of $H_d(\omega)$

$$\begin{aligned} x(n) &= \frac{1}{2\pi} \int_{-\pi}^{\pi} X(\omega) e^{j\omega n} d\omega = \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{j\omega n} d\omega \\ &= \frac{\omega_c}{\pi} \frac{\sin \omega_c n}{\omega_c n} \end{aligned}$$

+ Delayed impulse response (to make it causal)


$$\tilde{h}(n) = \hat{h}\left(n - \frac{N-1}{2}\right)$$

→ Coefficients of the ideal filter (via equation or IFFT):

$$h(n) = \frac{\sin(0.5\pi(n - 40))}{\pi(n - 40)}$$



Windowed Filter Design Example:
Step 4: Multiply to obtain the filter coefficients


$$h(n) = \frac{\sin(0.5\pi(n - 40))}{\pi(n - 40)}$$

- Multiply by a Hamming window function for the passband:

$$w(n) = 0.54 - 0.46 \cos\left(\frac{2\pi n}{M}\right)$$



Windowed Filter Design Example:
Step 5: Evaluate the Frequency Response and Iterate

- The frequency response is computed as the DFT of the filter coefficient vector
- **If** the resulting filter does not meet the specifications, **then**:
 - Adjust the ideal filter frequency response (for example, move the band edge) and repeat (step 2)
 - Adjust the filter length and repeat (step 4)
 - change the window (& filter length) (step 4)
- And/Or consult with Matlab:
 - **FIR1** and **FIR2**
 - **B=FIR2(N,F,M)** : Designs a Nth order FIR digital filter with



Windowed Filter Design Example: Consulting Matlab:

- **FIR1** and **FIR2**
 - **B=FIR2 (N, F, M)** : Designs a Nth order FIR digital filter
 - **F** and **M** specify frequency and magnitude breakpoints for the filter such that **plot(N,F,M)** shows a plot of desired frequency
 - Frequencies **F** must be in increasing order between 0 and $F_s/2$, with F_s corresponding to the sample rate.
 - **B** is the vector of length $N+1$, it is real, has linear phase and symmetric coefficients
 - Default window is Hamming – others can be specified



In Conclusion

- FIR Filters are digital (can not be implemented in analog) and exploit the difference and delay operators
- A window based design builds on the notion of a truncation of the “ideal” box-car or rectangular low-pass filter in the Frequency domain (which is a sinc function in the time domain)
- Other Design Methods exist:
 - Least-Square Design
 - Equiripple Design
 - Remez method
 - The Parks-McClellan Remez algorithm
 - Optimisation routines ...

