

This exam has THREE (3) Sections for a total of 100 Points

Section 1: Linear Signals & Systems	25 %
Section 2: Signal Processing	30 %
Section 3: Digital Control.....	45 %

Please answer **ALL** questions.

⇒ **PLEASE RECORD ALL ANSWERS IN THE ANSWER BOOKLET** ⇐

Any material not in Answer Booklet(s) **will not be seen**. In particular, the exam paper **will not be graded** or reviewed.

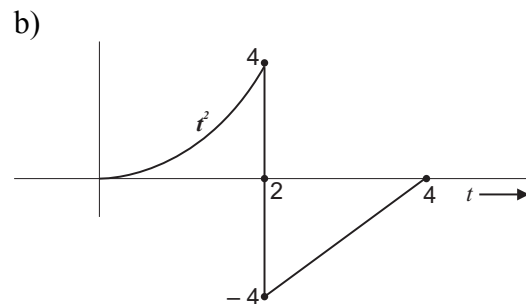
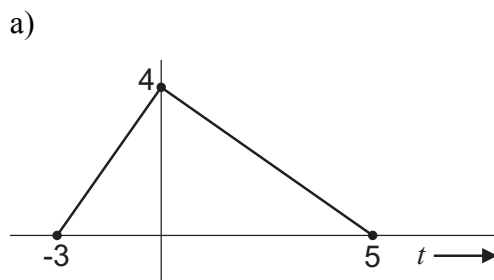
Section 1: Linear Signals & Systems

Please Record Answers in the **Answer Book**

(Total: **25%**)

1. **Whatchamacallit?** (5%)

Express the signals in the figure below by a single expression valid for all t .



2. **A Fast and E-Z Fourier** (5%)

Given a discrete-time **unit impulse response** with the following difference equation:

$$y[n] = \delta[n - 3] - \delta[n + 0] - \delta[n + 0] + \delta[n + 4]$$

- What is its Z-transform?
(i.e., what is $Y(z)$)?
- What is its frequency (or Fourier) response?
(i.e., what is $Y(\omega)$)
[hint: for partial credit, you may leave it in terms of the phasor $e^{j\omega}$]

3. **Is Digital Really Better?**

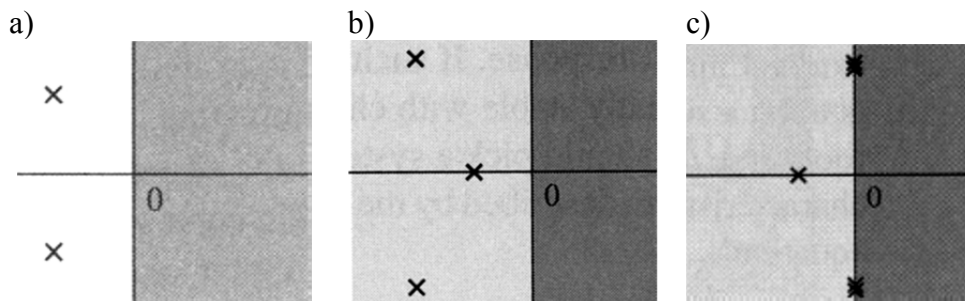
(5%)

- a) Briefly give TWO advantages of digital signals over analogue signals?
- b) Briefly give TWO advantages of analogue signals over digital signals?

4. **Characteristic Roots and Characteristic Modes**

(5%)

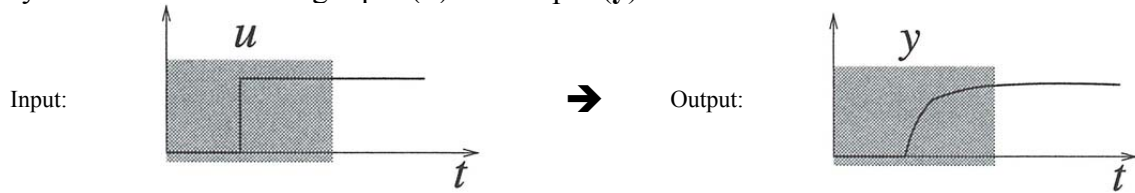
For systems having the following pole-zero plots (on the **s-plane**), please sketch the corresponding zero-input response.



5. I Spy LTI?

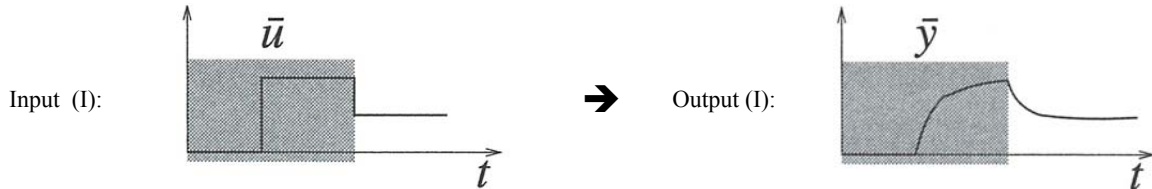
(5%)

A system has the following input (u) and output (y) relation.

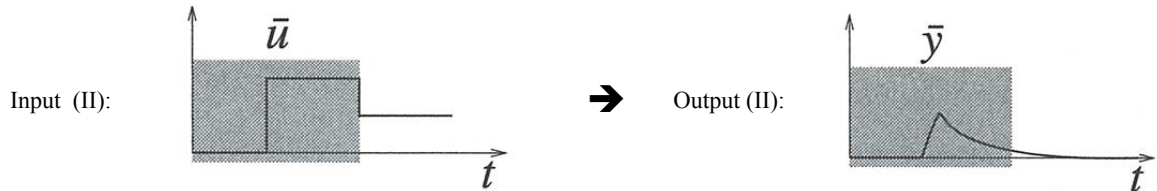


Suppose, for three different (and separate) cases the input is slightly varied as below.

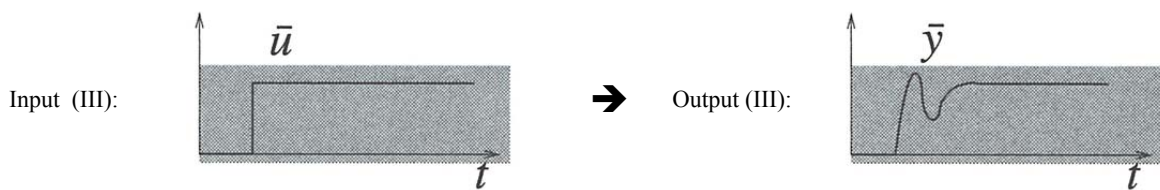
CASE I:



CASE II:



CASE III:



Please determine if the conditions can or cannot be determined. If it can be determined, then please state if it is or is not the case (please mark a \times in the table **[in the booklet!!]**)

[Note: Please treat each case separately. That is Case I is independent of Case II]

For CASE I, is the system:

	Yes	No	Indeterminate
Linear			
Time-Invariant			
Causal			

For CASE II, is the system:

	Yes	No	Indeterminate
Linear			
Time-Invariant			
Causal			

For CASE III, is the system:

	Yes	No	Indeterminate
Linear			
Time-Invariant			
Causal			

Section 2: Signal ProcessingPlease Record Answers in the **Answer Book**(Total: **30%**)**6. Battle of the Band(limited) Signals**

(5%)

A signal $f(t)$ is bandlimited to **B** Hz.Show that the signal $f(t)^n$ is bandlimited to **nB** Hz.[Hint: Start with $n=2$. Use frequency convolution property and the width property of convolution.]**7. Cogito Ergo Sum**

(5%)

a) **Briefly explain** (and/or show a simple sketch) what is meant by the terms *ergodic* and *ensemble* in the context of multiple stochastic digital samples or signals?

b) Does the noise have to be “white” for the system to remain unbiased?

(please **briefly explain**)

[Hint: what happens when “pink” noise is averaged?]

8. An Analogue to Filtering

(5%)

Consider a filter given by the following transfer function

$$H(s) = \frac{4\pi}{s + 4\pi}$$

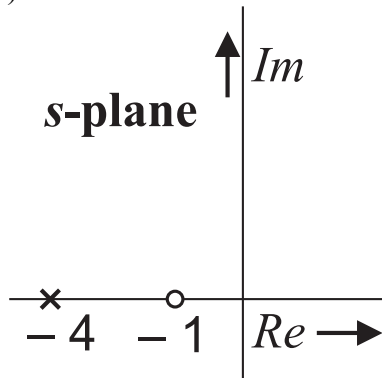
a) What is the order of $H(s)$?b) What is the cut-off frequency of $H(s)$?c) Design a low-pass digital filter, $H(z)$, with a sampling frequency of 100 Hz, that has the same cut-off frequency as $H(s)$.

9. A Filtered Whatchamacallit!

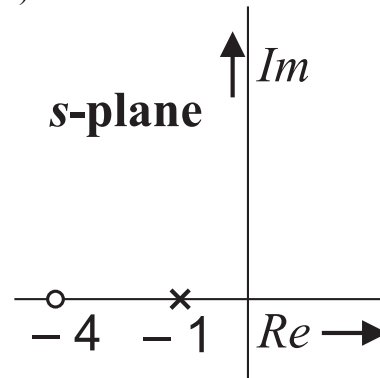
(5%)

What kind of compensator is described by pole-zero plots shown below. Please **briefly justify** the conclusion using a transfer function **and** a rough sketch of the amplitude and phase response of the filter.

a)



b)



10. A-Great Filter

(10%)

Design a high-pass filter for removing the **50 Hz** mains flicker from an audio signal from a guitar. The filter should have minimum transmission ≤ -120 dB (i.e., an approximate limit to human hearing). Also, the filter should not attenuate music signals from the note A-Great or higher (or more technically **110 Hz**, A_2 or “A”) by more -3 dB. **The filtered audio is then played to a concert musician live on stage.**

[Note: if you need to you may assume 24-bit, 44.1-kHz sampled signals if needed]

- What type of filter should we use (analogue or IIR or FIR)? (Please **justify**)
- What order does this filter need to be?
- Please sketch the frequency response of this filter.

Section 3: Digital Control

Please Record Answers in the **Answer Book**

(Total: **45%**)

11. A Discrete Convolution

(5%)

What is the convolution $(y_1 \otimes y_2)[n]$ between these discrete signals?

- a) $y_1[n]=\delta[n-3], y_2[n]=\delta[n+4]$
- b) $y_1[n]=\cos[2\pi n], y_2[n]=\delta[n-3]$

12. An E-Z Correspondence

(10%)

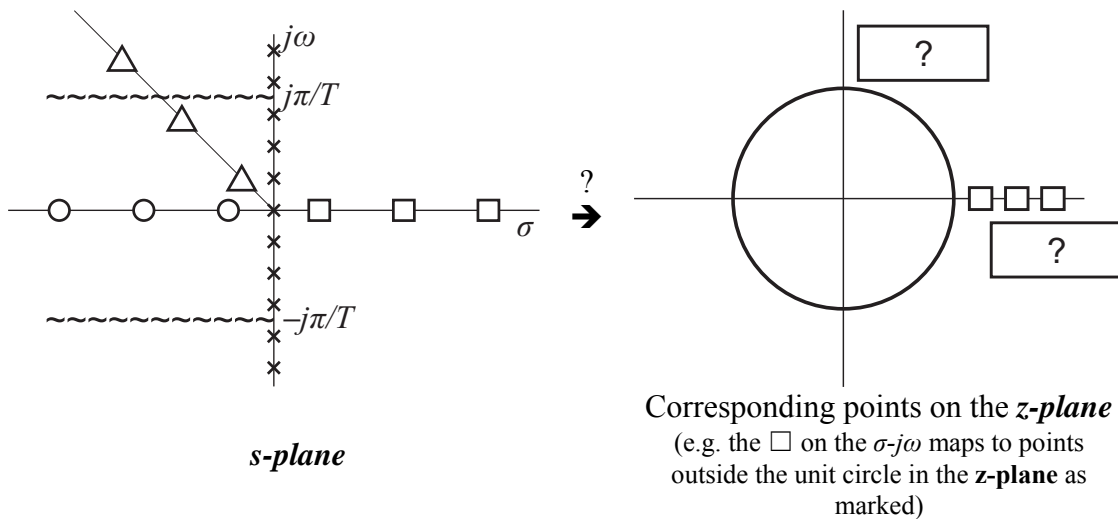
In mapping from the *s-plane* to the *z-plane*, recall that the duration of a time signal is related to the radius (of the pole location) and the sample rate is related to the angle by $z = e^{sT}$. From this we can sketch major features of the *s-plane* to the *z-plane* such that they have the same features.

For the following poles marked on the *s-plane*:

- a) “o”
- b) “Δ”
- c) “x”,
- d) “~”, and
- e) The axis labels (σ and $j\omega$)

please draw their corresponding locations (and/or terms) on the *z-plane*.

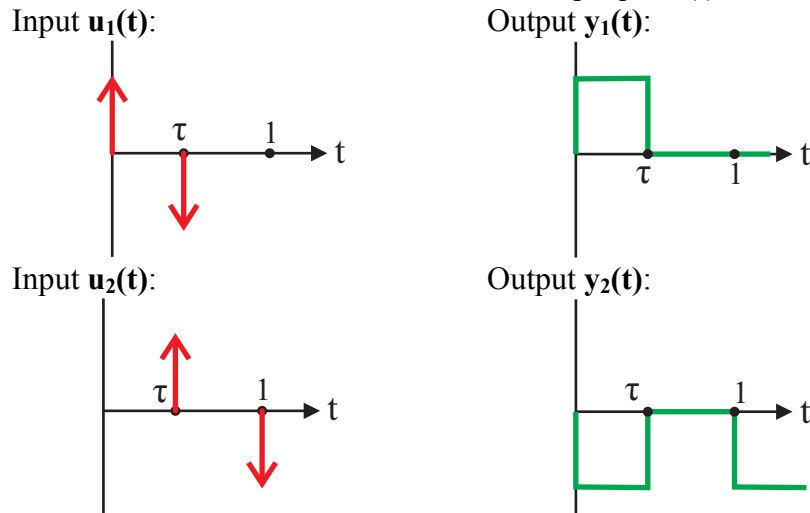
Please also **briefly justify** your mapping/answer.



13. Got LTI?

(10%)

A system consists of two blocks, with the following input $u(t)$ and output $y(t)$ pairs:



- a) Please provide a transfer function, $H_1(s)$ and $H_1(z)$ for y_1 given u_1 .
- b) Is the entire system (H_1H_2) LTI? (please briefly explain)
- c) If it is LTI, what is the order of the system?
If it is not LTI, what could be done to easily make it LTI?

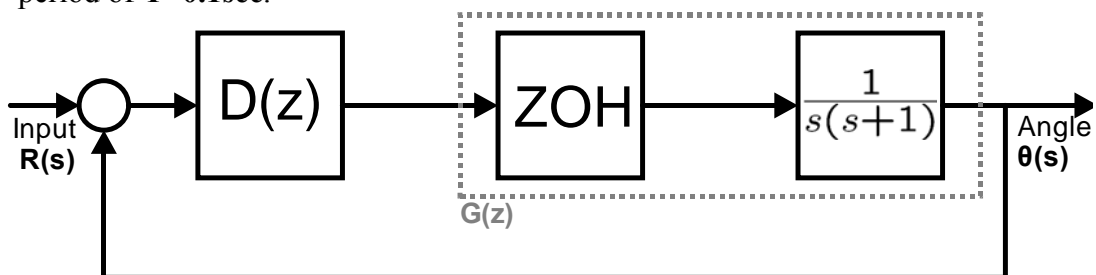
14. Steer-by-Wire

(10%)

A steer-by-wire system is proposed in which a DC motor regulates the hydraulic flow of a power steering system¹. It has the following continuous time plant

$$P(s) = \frac{1}{s(s + 1)}$$

The system is connected to a digital controller $D(z)$ by a ZOH process² having a period of $T=0.1\text{sec}$.



- a) Determine $G(z)$
[Hint: For this part you may leave it in terms of the z-Transform, $Z\{\bullet\}$ (i.e. $G(z)=Z\{G(s)\}$).
- b) Sketch the impulse response of $G(z)$

¹ Such systems are commercially available (often in very high-end vehicles) and should not be confused with all electric steer-by-wire systems (e.g. Nissan's Q50).

² Zero Order Hold. Recall that a ZOH is modelled by $G_{ZOH} = \frac{1-e^{-sT}}{s}$

15. One Last Stop on the ELEC3004 Express!

(10%)

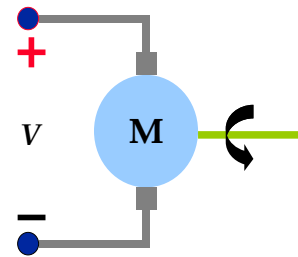
As part of an electric train, you need to implement a control system that stops a DC electric motor as fast as possible.

Recall that a DC motor is characterized by

$$v = k\omega + Ri + Li'$$

Where:

- v : the voltage at its electrical terminals
- i : the current
- i' : the time derivative of i (i.e. \dot{i})
- ω : shaft rotational speed (in rad/sec)
- R : resistance of the motor winding
- L : inductance of the motor winding
- k : motor constant



Recall that the torque is given by $\tau = ki$. The mechanical torque model is given by

$$J\omega' = -b\omega + \tau$$

To simplify exam calculations, assume unity values for all constants (with, of course, the appropriate physical units). Thus, $R=1$, $L=1$, $k=1$, $J=1$ and $b=1$.

Given that the motor has some initial speed when the brake is applied at $t=0$, $\omega(0)$, the task is to stop the motor. To do this, we throw a switch that disconnects the driving voltage and connects the terminals of the motor to a “stopping circuit”. One basic design for this is a big resistor, R_{Big} , resulting in

$$v_{stopping} = -R_{Big}i$$

- a) Derive a discrete transfer function from $\omega(0)$ to $v_{stopping}(z)$ for this plant, using the Tustin’s method.
- b) What is the slowest sampling rate that will not destabilise the system under unity-gain proportional negative feedback?
- c) Under what conditions can the inductance be ignored, and the motor treated as a single pole system?
- d) What value of R_{Big} results in the motor velocity stopping the fastest?
- e) Prof Gordian DuKnot suggests that the best thing to do is to set $R_{Big}=0$. That is, short circuit the motor. DuKnot’s argument is simple: “if more voltage makes it go faster, then less voltage makes it slower. Thus, zero voltage stops it.” Is this wise? (please **explain** your reasoning)

END OF EXAMINATION — Thank you !!!

Is the wonder still there? ☹

Table 1: Commonly used Formulae

The Laplace Transform

$$F(s) = \int_0^{\infty} f(t)e^{-st} dt$$

The \mathcal{Z} Transform

$$F(z) = \sum_{n=0}^{\infty} f[n]z^{-n}$$

IIR Filter Pre-warp

$$\omega_a = \frac{2}{\Delta t} \tan\left(\frac{\omega_d \Delta t}{2}\right)$$

Bi-linear Transform

$$s = \frac{2(1 - z^{-1})}{\Delta t(1 + z^{-1})}$$

FIR Filter Coefficients

$$c_n = \frac{\Delta t}{\pi} \int_0^{\pi/\Delta t} H_d(\omega) \cos(n\omega\Delta t) d\omega$$

Table 2: Comparison of Fourier representations.

<i>Time Domain</i>	Periodic	Non-periodic	
	Discrete Fourier Transform	Discrete-Time Fourier Transform	
Discrete	$\tilde{X}[k] = \frac{1}{N} \sum_{n=0}^{N-1} \tilde{x}[n]e^{-j2\pi kn/N}$ $\tilde{x}[n] = \sum_{k=0}^{N-1} \tilde{X}[k]e^{j2\pi kn/N}$	$X(e^{j\omega}) = \sum_{n=-\infty}^{\infty} x[n]e^{-j\omega n}$ $x[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{j\omega})e^{j\omega n} d\omega$	Periodic
	Complex Fourier Series	Fourier Transform	
Continuous	$X[k] = \frac{1}{T} \int_{-T/2}^{T/2} \tilde{x}(t)e^{-j2\pi kt/T} dt$ $\tilde{x}(t) = \sum_{k=-\infty}^{\infty} X[k]e^{j2\pi kt/T}$	$X(j\omega) = \int_{-\infty}^{\infty} x(t)e^{-j\omega t} dt$ $x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(j\omega)e^{j\omega t} d\omega$	Non-periodic
	Discrete	Continuous	Freq. Domain

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Table 3: Selected Fourier, Laplace and z -transform pairs.

Signal	\longleftrightarrow	Transform	ROC
$\tilde{x}[n] = \sum_{p=-\infty}^{\infty} \delta[n - pN]$	\xleftrightarrow{DFT}	$\tilde{X}[k] = \frac{1}{N}$	
$x[n] = \delta[n]$	\xleftrightarrow{DTFT}	$X(e^{j\omega}) = 1$	
$\tilde{x}(t) = \sum_{p=-\infty}^{\infty} \delta(t - pT)$	\xleftrightarrow{FS}	$X[k] = \frac{1}{T}$	
$\delta_T[t] = \sum_{p=-\infty}^{\infty} \delta(t - pT)$	\xleftrightarrow{FT}	$X(j\omega) = \frac{2\pi}{T} \sum_{k=-\infty}^{\infty} \delta(\omega - k\omega_0)$	
$\cos(\omega_0 t)$	\xleftrightarrow{FT}	$X(j\omega) = \pi\delta(\omega - \omega_0) + \pi\delta(\omega + \omega_0)$	
$\sin(\omega_0 t)$	\xleftrightarrow{FT}	$X(j\omega) = j\pi\delta(\omega + \omega_0) - j\pi\delta(\omega - \omega_0)$	
$x(t) = \begin{cases} 1 & \text{when } t \leq T_0, \\ 0 & \text{otherwise.} \end{cases}$	\xleftrightarrow{FT}	$X(j\omega) = \frac{2\sin(\omega T_0)}{\omega}$	
$x(t) = \frac{1}{\pi t} \sin(\omega_c t)$	\xleftrightarrow{FT}	$X(j\omega) = \begin{cases} 1 & \text{when } \omega \leq \omega_c , \\ 0 & \text{otherwise.} \end{cases}$	
$x(t) = \delta(t)$	\xleftrightarrow{FT}	$X(j\omega) = 1$	
$x(t) = \delta(t - t_0)$	\xleftrightarrow{FT}	$X(j\omega) = e^{-j\omega t_0}$	
$x(t) = u(t)$	\xleftrightarrow{FT}	$X(j\omega) = \pi\delta(\omega) + \frac{1}{j\omega}$	
$x[n] = \frac{\omega_c}{\pi} \text{sinc } \omega_c n$	\xleftrightarrow{DTFT}	$X(e^{j\omega}) = \begin{cases} 1 & \text{when } \omega < \omega_c , \\ 0 & \text{otherwise.} \end{cases}$	
$x(t) = \delta(t)$	$\xleftrightarrow{\mathcal{L}}$	$X(s) = 1$	all s
(unit step) $x(t) = u(t)$	$\xleftrightarrow{\mathcal{L}}$	$X(s) = \frac{1}{s}$	
(unit ramp) $x(t) = t$	$\xleftrightarrow{\mathcal{L}}$	$X(s) = \frac{1}{s^2}$	
$x(t) = \sin(s_0 t)$	$\xleftrightarrow{\mathcal{L}}$	$X(s) = \frac{s_0}{(s^2 + s_0^2)}$	
$x(t) = \cos(s_0 t)$	$\xleftrightarrow{\mathcal{L}}$	$X(s) = \frac{s}{(s^2 + s_0^2)}$	
$x(t) = e^{s_0 t} u(t)$	$\xleftrightarrow{\mathcal{L}}$	$X(s) = \frac{1}{s - s_0}$	$\Re\{s\} > \Re\{s_0\}$
$x[n] = \delta[n]$	$\xleftrightarrow{\mathcal{Z}}$	$X(z) = 1$	all z
$x[n] = \delta[n - m]$	$\xleftrightarrow{\mathcal{Z}}$	$X(z) = z^{-m}$	
$x[n] = u[n]$	$\xleftrightarrow{\mathcal{Z}}$	$X(z) = \frac{z}{z - 1}$	
$x[n] = z_0^n u[n]$	$\xleftrightarrow{\mathcal{Z}}$	$X(z) = \frac{1}{1 - z_0 z^{-1}}$	$ z > z_0 $
$x[n] = -z_0^n u[-n - 1]$	$\xleftrightarrow{\mathcal{Z}}$	$X(z) = \frac{1}{1 - z_0 z^{-1}}$	$ z < z_0 $
$x[n] = a^n u[n]$	$\xleftrightarrow{\mathcal{Z}}$	$X(z) = \frac{z}{z - a}$	$ z < a $

Table 4: Properties of the Discrete-time Fourier Transform.

Property	Time domain	Frequency domain
Linearity	$ax_1[n] + bx_2[n]$	$aX_1(e^{j\omega}) + bX_2(e^{j\omega})$
Differentiation (frequency)	$nx[n]$	$j \frac{dX(e^{j\omega})}{d\omega}$
Time-shift	$x[n - n_0]$	$e^{-j\omega n_0} X(e^{j\omega})$
Frequency-shift	$e^{j\omega_0 n} x[n]$	$X(e^{j(\omega - \omega_0)})$
Convolution	$x_1[n] * x_2[n]$	$X_1(e^{j\omega}) X_2(e^{j\omega})$
Modulation	$x_1[n] x_2[n]$	$\frac{1}{2\pi} X_1(e^{j\omega}) \otimes X_2(e^{j\omega})$
Time-reversal	$x[-n]$	$X(e^{-j\omega})$
Conjugation	$x^*[n]$	$X^*(e^{-j\omega})$
Symmetry (real)	$\Im\{x[n]\} = 0$	$X(e^{j\omega}) = X^*(e^{-j\omega})$
Symmetry (imag)	$\Re\{x[n]\} = 0$	$X(e^{j\omega}) = -X^*(e^{-j\omega})$
Parseval	$\sum_{n=-\infty}^{\infty} x[n] ^2 = \frac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) ^2 d\omega$	

Table 5: Properties of the Fourier series.

Property	Time domain	Frequency domain
Linearity	$a\tilde{x}_1(t) + b\tilde{x}_2(t)$	$aX_1[k] + bX_2[k]$
Differentiation (time)	$\frac{d\tilde{x}(t)}{dt}$	$\frac{j2\pi k}{T} X[k]$
Time-shift	$\tilde{x}(t - t_0)$	$e^{-j2\pi kt_0/T} X[k]$
Frequency-shift	$e^{j2\pi k_0 t/T} \tilde{x}(t)$	$X[k - k_0]$
Convolution	$\tilde{x}_1(t) \otimes \tilde{x}_2(t)$	$T X_1[k] X_2[k]$
Modulation	$\tilde{x}_1(t) \tilde{x}_2(t)$	$X_1[k] * X_2[k]$
Time-reversal	$\tilde{x}(-t)$	$X[-k]$
Conjugation	$\tilde{x}^*(t)$	$X^*[-k]$
Symmetry (real)	$\Im\{\tilde{x}(t)\} = 0$	$X[k] = X^*[-k]$
Symmetry (imag)	$\Re\{\tilde{x}(t)\} = 0$	$X[k] = -X^*[-k]$
Parseval	$\frac{1}{T} \int_{-T/2}^{T/2} \tilde{x}(t) ^2 dt = \sum_{k=-\infty}^{\infty} X[k] ^2$	

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Table 6: Properties of the Fourier transform.

Property	Time domain	Frequency domain
Linearity	$a\tilde{x}_1(t) + b\tilde{x}_2(t)$	$aX_1(j\omega) + bX_2(j\omega)$
Duality	$X(jt)$	$2\pi x(-\omega)$
Differentiation	$\frac{dx(t)}{dt}$	$j\omega X(j\omega)$
Integration	$\int_{-\infty}^t x(\tau) d\tau$	$\frac{1}{j\omega} X(j\omega) + \pi X(j0)\delta(\omega)$
Time-shift	$x(t - t_0)$	$e^{-j\omega t_0} X(j\omega)$
Frequency-shift	$e^{j\omega_0 t} x(t)$	$X(j(\omega - \omega_0))$
Convolution	$x_1(t) * x_2(t)$	$X_1(j\omega)X_2(j\omega)$
Modulation	$x_1(t)x_2(t)$	$\frac{1}{2\pi} X_1(j\omega) * X_2(j\omega)$
Time-reversal	$x(-t)$	$X(-j\omega)$
Conjugation	$x^*(t)$	$X^*(-j\omega)$
Symmetry (real)	$\Im\{x(t)\} = 0$	$X(j\omega) = X^*(-j\omega)$
Symmetry (imag)	$\Re\{x(t)\} = 0$	$X(j\omega) = -X^*(-j\omega)$
Scaling	$x(at)$	$\frac{1}{ a } X\left(\frac{j\omega}{a}\right)$
Parseval	$\int_{-\infty}^{\infty} x(t) ^2 dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(j\omega) ^2 d\omega$	

Table 7: Properties of the z -transform.

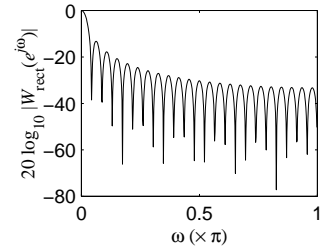
Property	Time domain	z -domain	ROC
Linearity	$ax_1[n] + bx_2[n]$	$aX_1(z) + bX_2(z)$	$\subseteq R_{x_1} \cap R_{x_2}$
Time-shift	$x[n - n_0]$	$z^{-n_0} X(z)$	R_x^\dagger
Scaling in z	$z_0^n x[n]$	$X(z/z_0)$	$ z_0 R_x$
Differentiation in z	$nx[n]$	$-z \frac{dX(z)}{dz}$	R_x^\dagger
Time-reversal	$x[-n]$	$X(1/z)$	$1/R_x$
Conjugation	$x^*[n]$	$X^*(z^*)$	R_x
Symmetry (real)	$\Im\{x[n]\} = 0$	$X(z) = X^*(z^*)$	
Symmetry (imag)	$\Re\{X[n]\} = 0$	$X(z) = -X^*(z^*)$	
Convolution	$x_1[n] * x_2[n]$	$X_1(z)X_2(z)$	$\subseteq R_{x_1} \cap R_{x_2}$
Initial value	$x[n] = 0, n < 0 \Rightarrow x[0] = \lim_{z \rightarrow \infty} X(z)$		

$\dagger z = 0$ or $z = \infty$ may have been added or removed from the ROC.

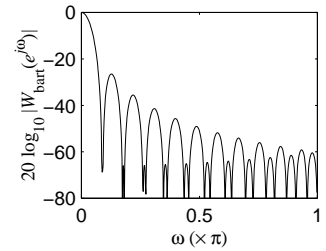
Table 8: Commonly used window functions.

Rectangular:

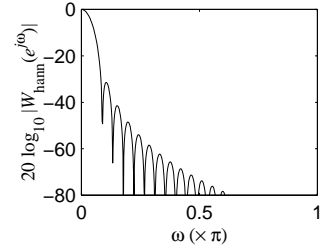
$$w_{\text{rect}}[n] = \begin{cases} 1 & \text{when } 0 \leq n \leq M, \\ 0 & \text{otherwise.} \end{cases}$$

*Bartlett (triangular):*

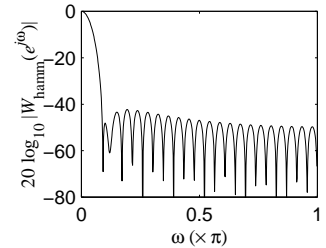
$$w_{\text{bart}}[n] = \begin{cases} 2n/M & \text{when } 0 \leq n \leq M/2, \\ 2 - 2n/M & \text{when } M/2 \leq n \leq M, \\ 0 & \text{otherwise.} \end{cases}$$

*Hanning:*

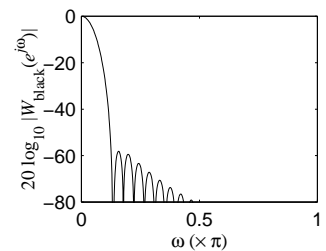
$$w_{\text{hann}}[n] = \begin{cases} \frac{1}{2} - \frac{1}{2} \cos(2\pi n/M) & \text{when } 0 \leq n \leq M, \\ 0 & \text{otherwise.} \end{cases}$$

*Hamming:*

$$w_{\text{hamm}}[n] = \begin{cases} 0.54 - 0.46 \cos(2\pi n/M) & \text{when } 0 \leq n \leq M, \\ 0 & \text{otherwise.} \end{cases}$$

*Blackman:*

$$w_{\text{black}}[n] = \begin{cases} 0.42 - 0.5 \cos(2\pi n/M) \\ \quad + 0.08 \cos(4\pi n/M) & \text{when } 0 \leq n \leq M, \\ 0 & \text{otherwise.} \end{cases}$$



Type of Window	Peak Side-Lobe Amplitude (Relative; dB)	Approximate Width of Main Lobe	Peak Approximation Error, $20 \log_{10} \delta$ (dB)
Rectangular	-13	$4\pi/(M+1)$	-21
Bartlett	-25	$8\pi/M$	-25
Hanning	-31	$8\pi/M$	-44
Hamming	-41	$8\pi/M$	-53
Blackman	-57	$12\pi/M$	-74